DRAINAGE REPORT

To Accompany Development Plan For The Lost Creek ISR Facility

Prepared for:



August 2009



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Drainage Report for the Lost Creek ISR Facility

This report details the existing and proposed drainage patterns in and around the proposed facilities to be constructed at the Lost Creek mine site. These facilities will include the Process Plant, Drill Shop, and the intersection of the mine access road with the Wamsutter-Crooks Gap Road, Sweetwater County Road 23. The site is located approximately 34 miles north of Wamsutter, Wyoming and approximately 25 miles south of Jeffery City, Wyoming in the area known as the Great Divide Basin.

Existing Topography and Soil Conditions

The topography around the Lost Creek ISR Facility is relatively flat, with gently rolling slopes and small drainages. Existing vegetation around the entire area is native rangeland grasses and sagebrush. In a report by Inberg-Miller Engineers which was provided to us by UR Energy, the bore logs show primarily sandy clay on the surface. Beneath the surface layer is dense sandstone. Cursory geologic reviews indicate the Battle Spring Formation occurs at or near the surface in much of the eastern portion on the Great Divide Basin. The Battle Spring Formation is composed of sandstone, with lesser amounts of clay and mudstone. The Battle Spring Formation has good water-bearing properties, which indicates that its runoff potential would be minimal. Inspection of topographic maps in the subject area indicates minimal topographic relief, with the majority of streams draining to playas.

Process Plant

The proposed Process Plant is located in Section 18, T25N, R92W. The existing topography around the plant generally flows to the south with very gentle slopes. The plant site is located just east of a small swale, with two proposed holding ponds located just east of the process plant in the bottom of the swale. The drainage area of the watershed above the plant site is approximately 350 acres. This drainage area was split into three basins: one basin that will drain to the north and west sides of the process plant, one basin that will drain to the north and east of the process plant between the process plant and holding ponds, and one basin that will drain into a diversion ditch around the east side of the holding ponds. The delineated drainage basins have been included on Sheet 1 of 7 of the Drainage Plan exhibits.

The existing drainage patterns will remain basically unchanged after construction of the process plant and holding ponds. The process plant itself will be constructed on a flat and level pad, with the surrounding parking and access areas sloping away from the building in all directions. The shop will be constructed on a flat and level pad to the north of the process plant. Drainage ditches will be constructed around the parking and access area to intercept and redirect runoff from the adjacent lands around and away from the building. The majority of runoff intercepted by the process plant will be coming form the northwest. Once intercepted by the ditches around the building, these flows will be diverted to the south until they have moved beyond the plant. Runoff in the swale upstream of the holding ponds will be diverted to flow around the holding ponds to the east, then return to the original flow path directly south of the holding ponds. All drainage basin calculations used the curve number 70, minimum infiltration rate of 0.15 in/hr, adjusted minimum infiltration rate of 2.2", 25 yr SCS Type II 24 hr-general storm. All ditch and culvert channel slopes are 0.005 ft/ft. Tables 1 and 2 show calculated values and geometric parameters for the drainage basins, ditches, and one culvert around the process plant, shop, and holding ponds:

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	MI^2	MI	FT	CFS	AC-FT
BASIN	DRAINAGE AREA	WATERCOURSE LENGTH	ELEV. DIFF.	PEAK DISCHARGE	RUNOFF VOLUME
PROCESS PLANT	0.0500	0.42	40	7.57	0.33
BETWEEN PLANT & PONDS	0.0070	0.21	15	1.93	0.07
POND AREA	0.4900	1.16	80	39.83	3.23

Table 1 Process Plant Area Drainage Basins

	FT:FT	FT:FT	FT	FT	IN
DESCRIPTION	LEFT SLOPE	RIGHT SLOPE	BOTTOM WIDTH	MIN. DEPTH	DIAMETER
NORTH & WEST PROCESS PLANT DITCH	5:1	3:1	5	2.0	
EMERGENCY ACCESS RD CULVERT					24
DITCH BETWEEN PLANT AND PONDS	3:1	4:1	0	1.5	
DIVERSION DITCH	3:1	3:1	10	3.0	

Table 2 Process Plant Area Ditches and Culvert Size

The emergency access road will intersect with the access road approximately 300' south of the gate, and will require a 24" corrugated metal pipe (CMP) culvert to pass the stormwater runoff from the north and west process plant ditch and the land area encompassed by the two roads. This intersection and culvert are not shown on the drainage plan sheets.

<u>Drill Shop</u>

The proposed drill shop is also located in Section 18, approximately 2000' south of the Process Plant. The drill shop will be constructed on top of a gently sloping ridge, just east of the swale where the holding ponds are located. There is no significant watershed above the drill shop, as surface runoff will tend to travel off either side of the ridge to the east and west. No significant change in drainage patterns is anticipated once construction of the drill shop and adjacent staging area has been completed. The topsoil will be stripped around the drill shop and staging area, and gravel will be placed in the staging area yard. A small foundation pad for the drill shop will be constructed. It will be elevated above the surrounding area by a minimum of one foot, with 3:1 or flatter fill slopes on all sides.

The drainage area for the drill shop culvert is approximately 0.0006 mi^2 with an elevation difference of 10' and a watercourse length of 0.1 mi. This basin creates a peak discharge of 0.15 cfs that will be transmitted through a culvert beneath the approach. Using open channel flow hydraulics and an estimated slope of 0.0045 ft/ft, a 12" CMP culvert will have adequate capacity to convey runoff from the 25-yr event.

Wamsutter Road Intersection with Lost Creek ISR Facility Access Road

A proposed access road to the Lost Creek ISR facility will be constructed from County Road 23, also known as the Wamsutter-Crooks Gap Road. A separate road design for this access road has been prepared. This report only pertains to the drainage around the intersection approach of these two roads. The access road intersection will be located in Section 16, T25N R93W. The existing Wamsutter-Crooks Gap Road runs basically north-south, with the proposed access road running east-west. Surface runoff in the area around this intersection flows generally from east to west, and is intercepted by the Wamsutter-Crooks Gap Road. The grade of the Wamsutter-Crooks Gap Road flows towards the north, although there is a small swale located just south of the proposed intersection.

Existing drainage patterns will remain unchanged after construction of the access road approach. Construction of this road will only change the location where runoff from this basin is intercepted by the Wamsutter-Crooks Gap Road. The only increase in runoff may occur from the difference in impervious soils between existing soils and the proposed roadway surface. Pre developed runoff estimates for the basin have been estimated at 2.47 cfs and 0.07 ac-ft; while post development increases are only estimated to be an additional 0.225 cfs and 0.013 ac-ft. The drainage area for the intersection is approximately 0.005 mi² with an elevation difference of 7' and a watercourse length of 0.1 mi. An 18" CMP culvert will be placed under the approach, and will convey the calculated 2.47 cfs runoff from the north side of the existing fence line under the approach where it will flow north in the borrow ditch along the Wamsutter-Crooks Gap Road, as it does currently.

No changes will occur to the drainage patterns or the drainage areas south of the access road approach after construction of the access road. Runoff south of the existing fence line will be intercepted by the borrow ditch and will flow south to the existing swale where it will collect on the east side of Wamsutter road. It should be noted that there was not an existing culvert visible under the Wamsutter-Crooks Gap Road to convey this runoff to the west side of the road, where it could continue flowing west in the existing drainage channel.

ATTACHMENT A

HYDRAULIC CALCULATIONS

Trihydo-98

UR Energy Drill Shop Culvert Basin SCS Type II, 24-Hour General Storm

25-Year Return Period

Basin Characteristics		
Drainage Area (A)	0.0006 squa	are miles
Stream Length of Longest Watercours	0.100 m:	iles
Elevation Difference of Watercourse	10.000 fe	eet
Runoff Curve Number (CN)	70.000	
Minimum Infiltration Loss (iph)	0.150	
inches/hour		
Precipitation for Specified Storm		
Adjusted Precipitation for Selected	2.200 in	nches
Resultant Hydrograph Values		
Peak Discharge	0.20 ci	fs
Runoff Volume	0.00 ad	cre-feet
Time to Peak Discharge	12.00 ho	ours
Time of Concentration	0.01 h	ours

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Circular	Channel: Manni	ng's Equation - UR Ener	ะสภ
omment: Drill Shop G	ulvert		
Solve ForBuilt	Plow Diameter		
Diameter	ft ft	Velocity	fps
Slope Manning's n	0.0095 ft/ft 0.026	Flow Area Critical Slope	st ft/ft
Discharge	0.026 0.15 cfs ft	Critical Depth Percent Full.	ft
Depth	IC	Froude Number.	
		Full Capacity. OMAX 0.94D	cfs cfs
		4.000 CT/ 10	
	li kela <u>na sedana</u>		

A 12" CMP culvert will suffice since 75% of the Peak Discharge can be passed by a CMP culvert less than 6" in diameter on a very flat slope. The 12" diameter culvert has 4 times to area to pass the flow.

Trihydo-98

UR Energy Process Plant SCS Type II, 24-Hour General Storm 25-Year Return Period

Basin Characteristics		
Drainage Area (A)	0.050 s	quare miles
Stream Length of Longest Watercours	0.420	miles
Elevation Difference of Watercourse	40.000	feet
Runoff Curve Number (CN)	70.000	
Minimum Infiltration Loss (iph)	0.150	
inches/hour		
Precipitation for Specified Storm		
Adjusted Precipitation for Selected	2.200	inches
Resultant Hydrograph Values		
Peak Discharge	7.57	cfs
Runoff Volume	0.33	acre-feet
Time to Peak Discharge	12.22	hours
Time of Concentration	0.32	hours

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Circular	Channel: Manni	ng's Equation - UR Ener	. 87
omment: <u>Emergency A</u> Solve For	Real Real Program in the second second		
Diameter Slope Manning's n Discharge Depth	ft 1.0050 ft/ft 1.0050 ft/ft 1.005 1.005 ft	Velocity Flow Area Critical Slope Critical Depth Percent Full Froude Number. Full Capacity. QMAX 0.94D	fps sf ft/ft ft % cfs cfs

Need at least a 2 ft CMP culvert to handle the flow under the emergency access road near the Process Plant.

	ad Methods Flow —— Trapezoida	Master I version 3.21 1 - UR Energy	
Comment: <u>Process Pla</u> Solve For			
Bottom Width Lt Side Slope Rt Side Slope Manning's n Channel Slope Depth Discharge	ft ft ft/ft ft cfs	Velocity Flow Area Flow Top Width Wetted Perimeter Critical Depth Critical Slope Froude Number	fps sf ft ft ft ft/ft

This is new ditch geometry to keep the 25 yr event from approaching the building. Use for North and West ditches. A relatively large portion of the basin flows into the West ditch, so it is assumed that this 1 ft depth conveying approximately half of the 7.57 cfs will suffice for the North ditch.

Trihydo-98

UR Energy Wamsutter Road Approach SCS Type II, 24-Hour General Storm 25-Year Return Period Basin Characteristics Drainage Area (A) 0.010 square miles Stream Length of Longest Watercours 0.100 miles Elevation Difference of Watercourse 7.000 feet Runoff Curve Number (CN) 70.000 Minimum Infiltration Loss (iph) 0.150 inches/hour Precipitation for Specified Storm Adjusted Precipitation for Selected 2.200 inches Resultant Hydrograph Values Peak Discharge 2.47 cfs Runoff Volume 0.07 acre-feet Time to Peak Discharge 12.04 hours Time of Concentration 0.12 hours

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Circular (Channel: Manni	ng's Equation - UR Ener	an the second
Comment: Mamsutter Roa	ad Approach		
Solve ForPall	Flow Diameter		
Diameter Slope Manning's n Discharge Depth	ft ft/ft cfs ft	Velocity Flow Area Critical Slope Critical Depth Percent Full Froude Number. Full Capacity. QMAX 0.94D	fps sf ft/ft ft x cfs cfs

18" CMP will suffice.

Trihydo-98

UR Energy Pond Area

SCS Type II, 24-Hour General Storm 25-Year Return Period

Basin Characteristics	
Drainage Area (A)	0.490 square miles
Stream Length of Longest Watercours	1.160 miles
Elevation Difference of Watercourse	80.000 feet
Runoff Curve Number (CN)	70.000
Minimum Infiltration Loss (iph)	0.150
inches/hour	
Precipitation for Specified Storm	
Adjusted Precipitation for Selected	2.200 inches
Resultant Hydrograph Values	
Peak Discharge	39.83 cfs
Runoff Volume	3.23 acre-feet
Time to Peak Discharge	12.63 hours
Time of Concentration	0.80 hours

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Ponds	A DESCRIPTION OF THE REPORT OF THE
Uelocity (H:U) Flow Area (H:U) Flow Top Wid Wetted Perin ft/ft Critical Dep Critical Slo s Froude Numbe	th. sf heter ft oph. ft ope. ft/ft
	(H:U) Flow Area (H:U) Flow Top Wick Wetted Perin ft/ft Critical Dep Critical Slo

Need about a 3 ft deep trapezoidal channel with the above dimensions to route the natural drainage around the ponds in the Diversion Ditch.

Trihydo-98

UR Energy Ditch Between Process SCS Type II, 24-Hour Gener 25-Year Return Perio	al Storm
Basin Characteristics	
Drainage Area (A)	0.010 square miles
Stream Length of Longest Watercours	0.210 miles
Elevation Difference of Watercourse	15.000 feet
Runoff Curve Number (CN)	70.000
Minimum Infiltration Loss (iph)	0.150
inches/hour	
Precipitation for Specified Storm	
Adjusted Precipitation for Selected	2.200 inches
Resultant Hydrograph Values	
Peak Discharge	1.93 cfs
Runoff Volume	0.07 acre-feet
Time to Peak Discharge	12.10 hours
Time of Concentration	0.21 hours

Created 08/27/09 13:15:40 AUTHOR:

	—— Triangular	- UR Energy	
Comment: Between Pro		nds	
Solve ForDown Lt Side Slope Rt Side Slope Manning's n Channel Slope Depth Discharge	1 00:1 (H:U) 1 01:1 (H:U) 1 00:0 ft/ft 1 01:0 ft ft cfs	Velocity Flow Area Flow Top Width Wetted Perimeter Critical Depth Critical Slope Froude Number	fps sf ft ft ft ft/ft

Need 1.25 ft deep ditch between Process Plant and Ponds to contain the runoff.

e <u>N</u> otes <u>A</u> b	out						
Study Title UF	R Energy South Emergency Access Cu	lvert Basin	[
Author JA	J Notes						
English Metric	Watershed Location • West of the 105th Meridian	he 105th Meridian		Calculate		Plot	
mens	C East of the 105th Meridian	C. Gibe			Print		
Basin Chara	Decimal Places Inpi cteristics	ut 💶 🛌	Unit Hydrograph	Parameters	Decimal Place	s Output 🚺	
Drainage Are	a 0.0048 - (square	miles)	Unadjusted Time of	of Concentration	0.09	(Hr)	
Watercourse	Length 0.1278 : (miles)		Adjusted Time of C	Concentration	0.13	(Hr)	
Elevation Diff	erence 13.0000 ÷ (feet)		Duration of Excess	s Rainfall, D	0.02	(Hr)	
Infiltration Rat	te 0.1500 + (inches	/hour)	Time to Peak	Г	0.08	(Hr)	
Curve Number 70.0000 ÷		Base Time		0.22	(Hr)		
			QPeak (Peak Flow	v for Unit Hydrograph)	27.69	(cfs)	
Precipitation	Precipitation Distribution		Resultant Hydro	graph Values			
SCS Type II, 24-Hour General Storm			Peak Discharge		1.16	(cfs)	
			Runoff Volume		17.325	(acre-feet)	
Adjusted Precipitation Return Period			Time to Peak Discharge		12.04		

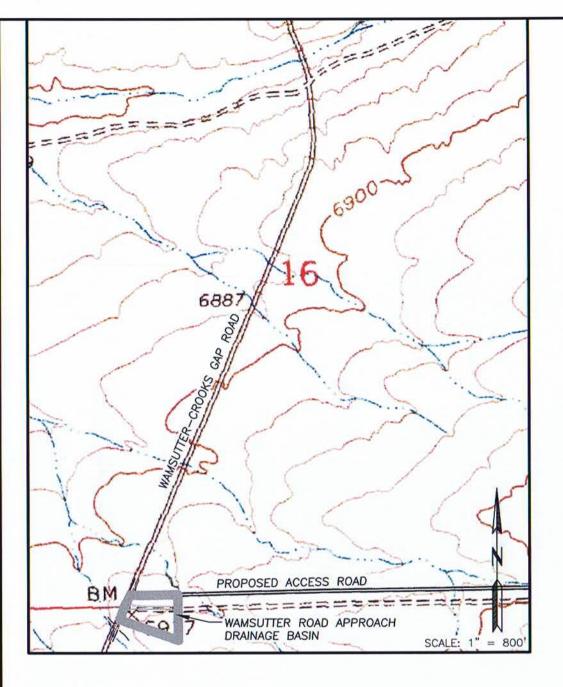
Add the 7.57 cfs peak discharge from the upstream Process Plant to get 8.71 cfs peak discharge total.

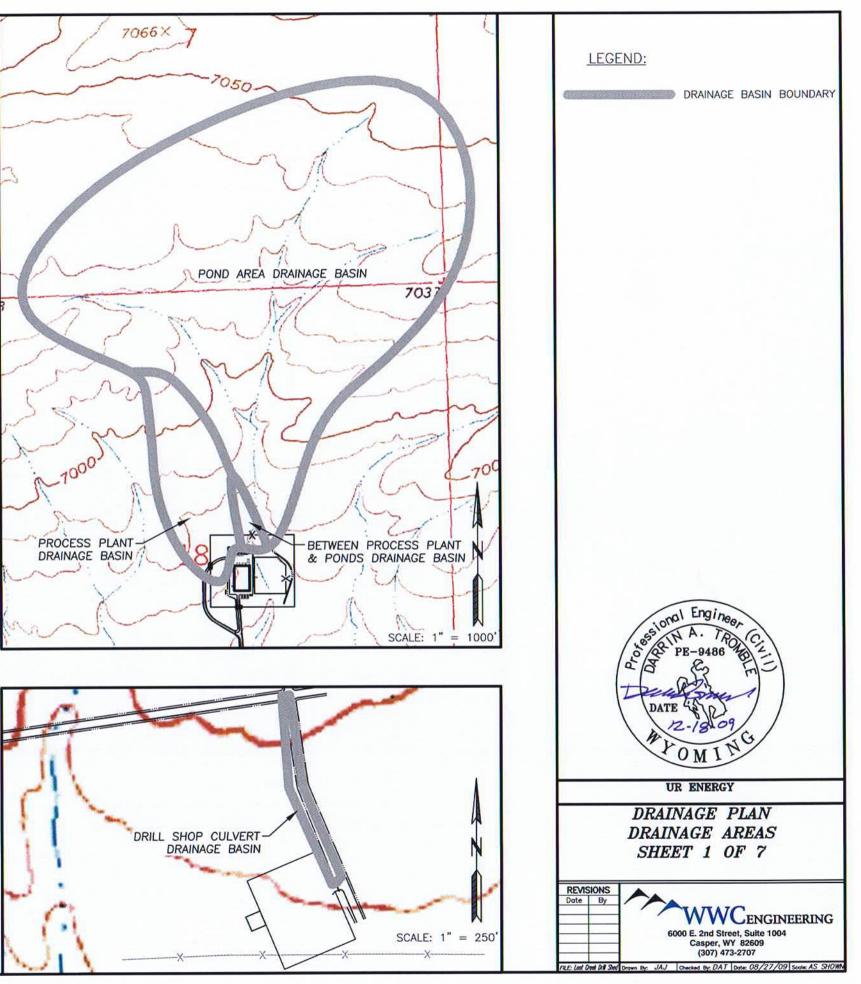
	shaw high will and :	Master I version 3.21	Diversion States and
Circular	Channel: Manni	ng's Equation - UR Ener	ray
omment: Emergency A	ccess Road Sout	h Culvert	
Solve ForRuid	Flow Diameter		
Diameter	ft 0.0240 ft/ft	Velocity	fps
Slope Manning's n	0.0240 ft/ft	Flow Area Critical Slope	sf ft/ft
Discharge	0-026 14.38 cfs	Critical Depth	👌 🔐 ft
Depth	t ft	Percent Full Froude Number.	2 2 %
		Full Capacity. QMAX 0.94D	cfs cfs
		41HA C.74D	CIS

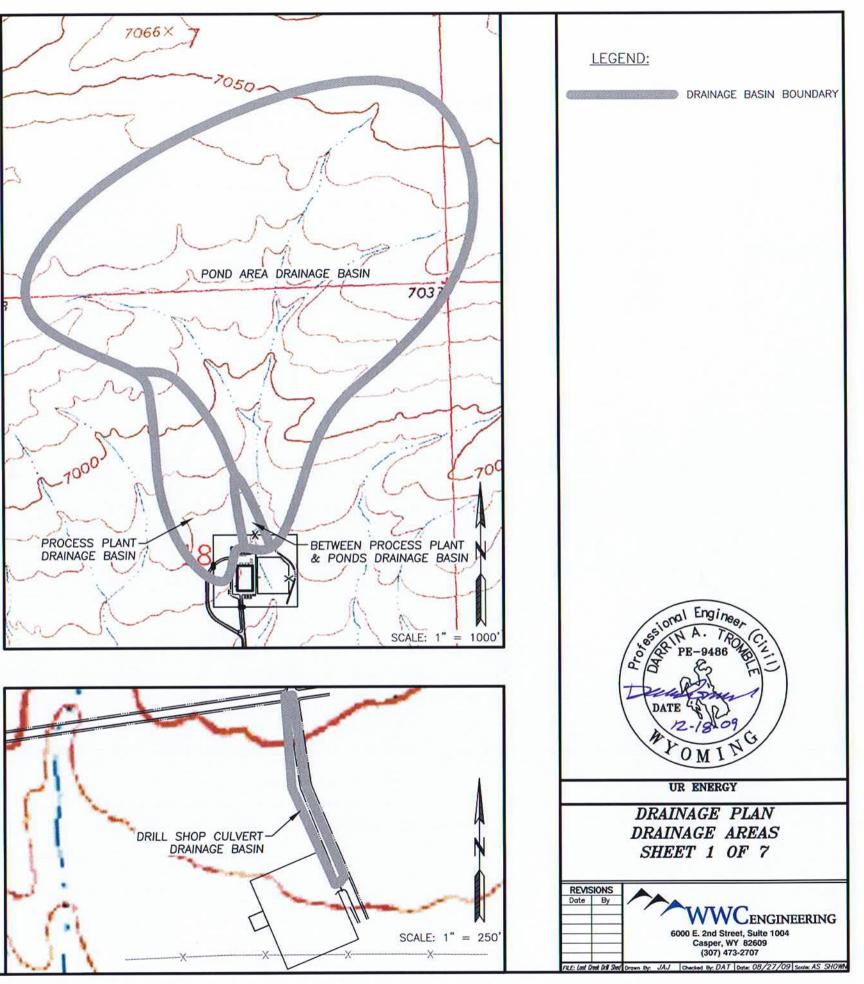
Need at least a 2 ft CMP culvert to handle the flow under the emergency access road south of the Process Plant. The 2 ft CMP can pass much more than 8.71 cfs.

ATTACHMENT **B**

DRAWINGS



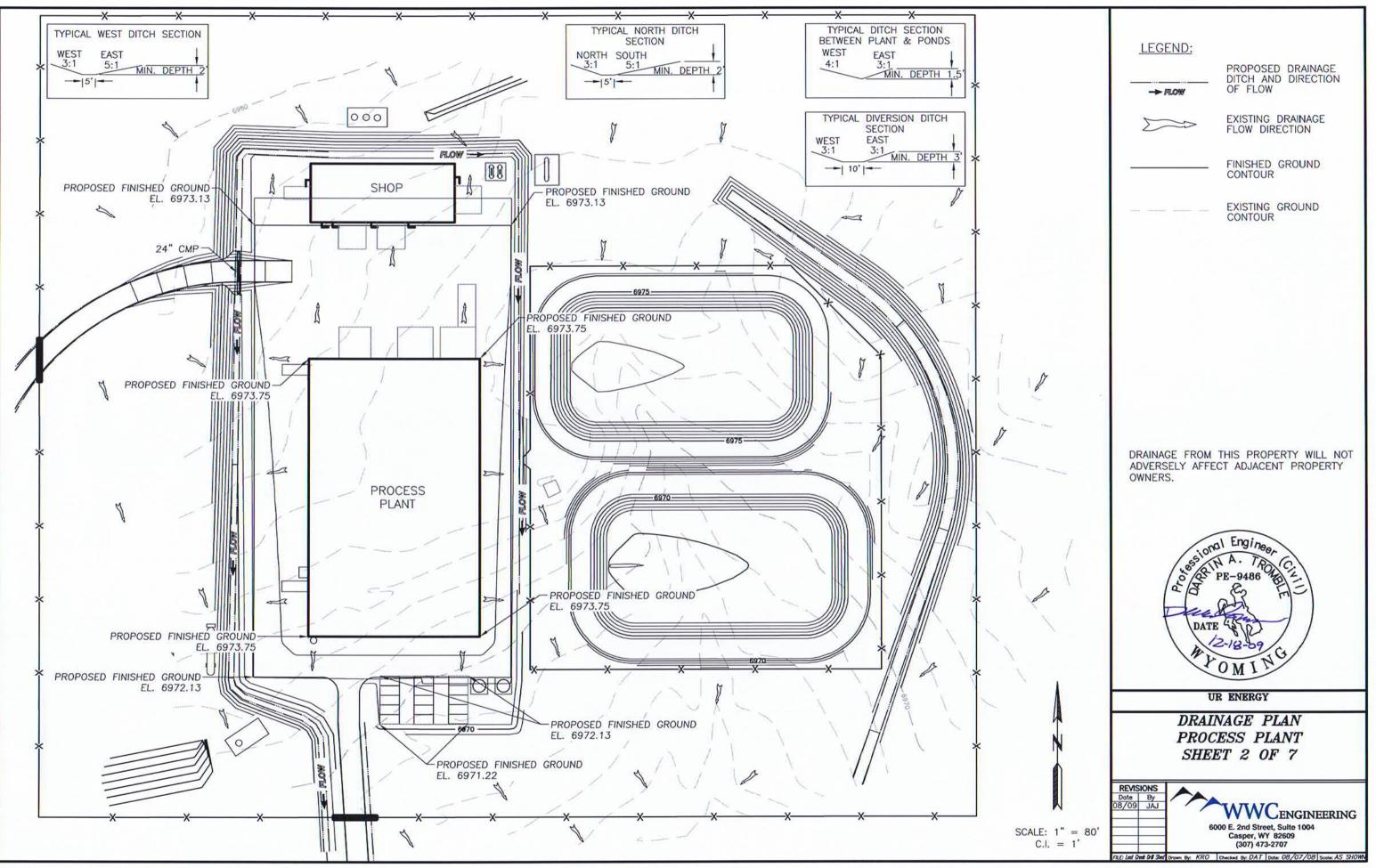


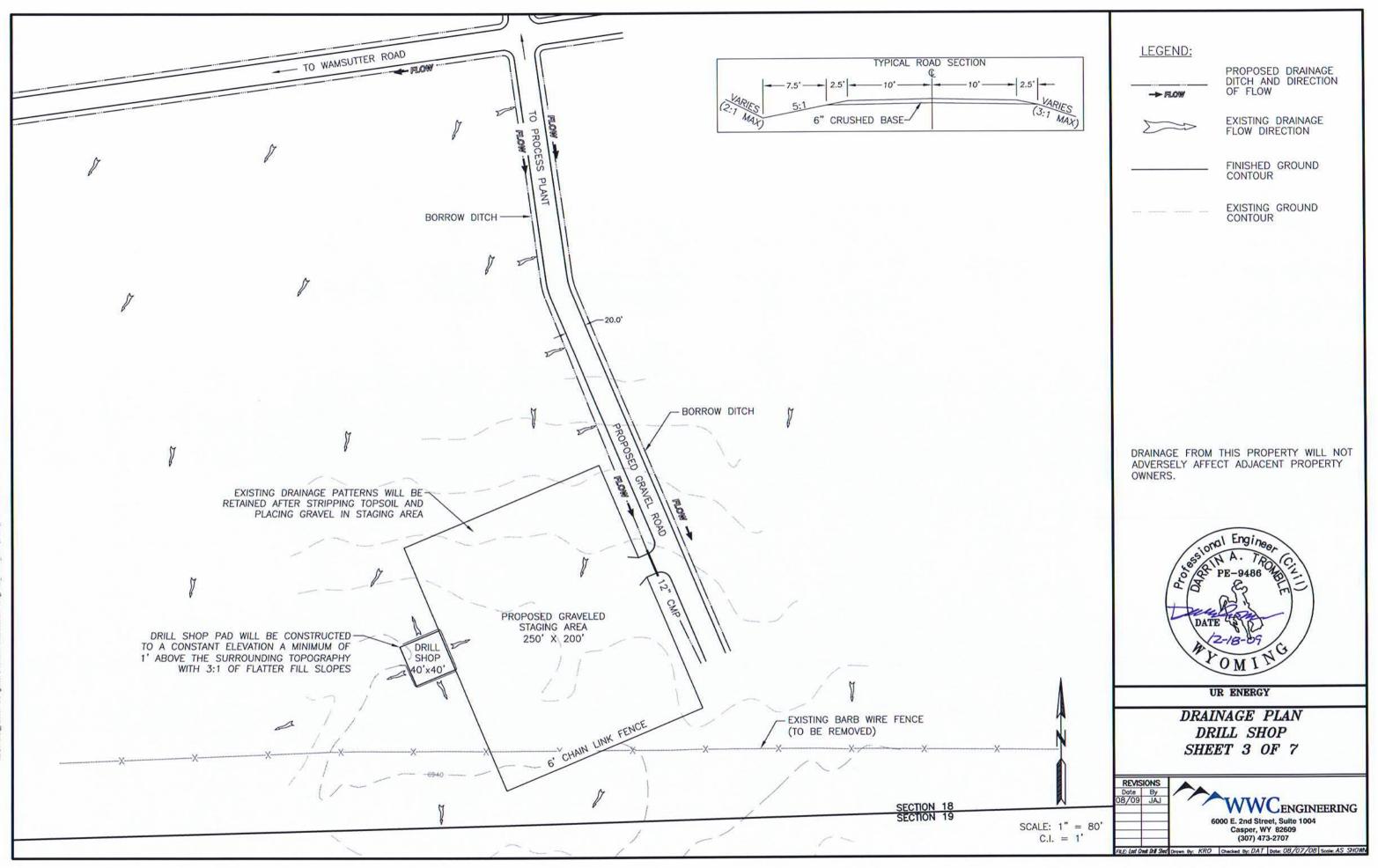


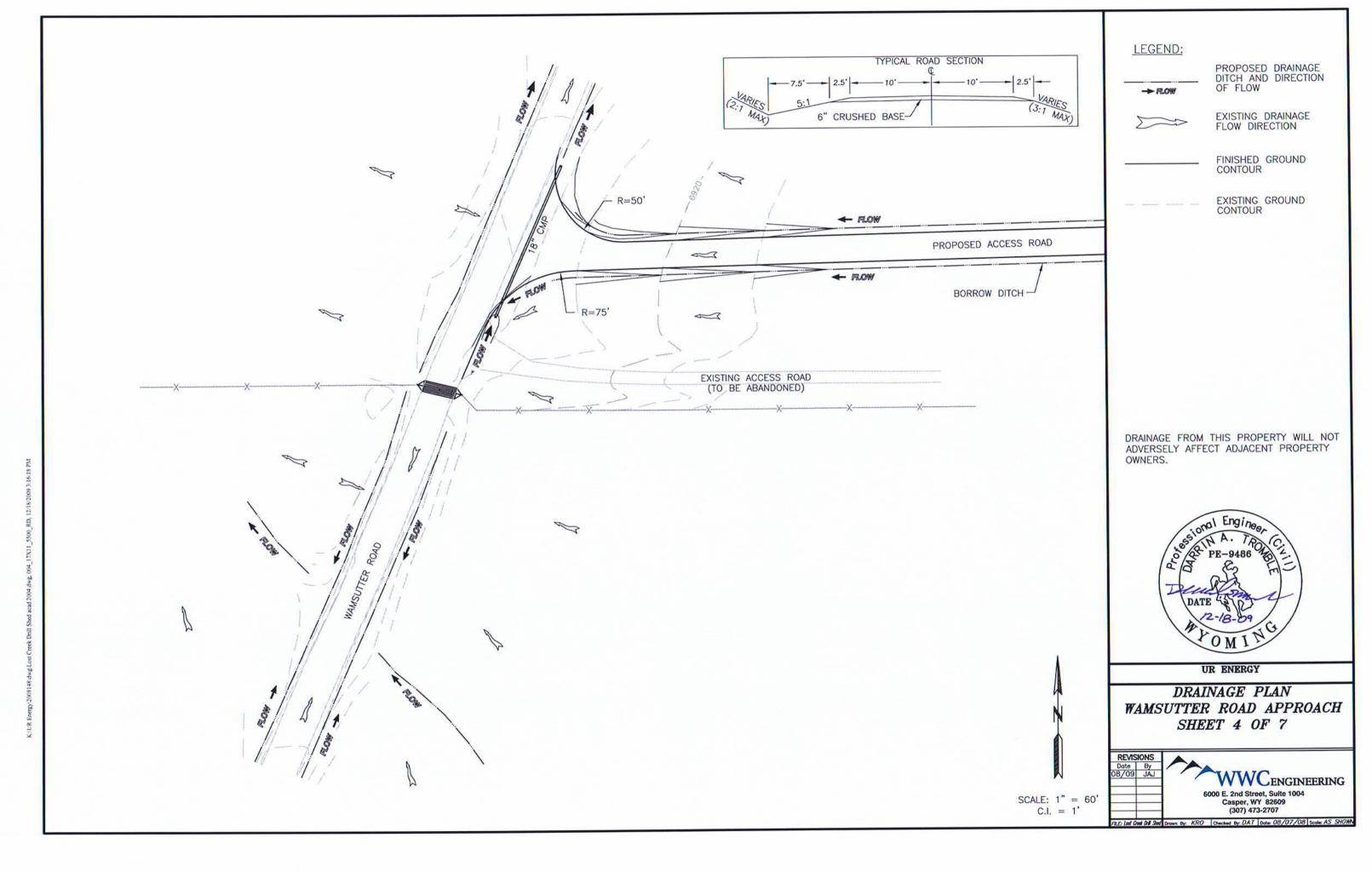
BASIN	MI ² DRAINAGE AREA	MI WATERCOURSE LENGTH	FT ELEV. DIFF.	CFS PEAK DISCHARGE	AC-FT RUNOFF VOLUME
PROCESS PLANT	0.0500	0.42	40	7.57	0.33
BETWEEN PLANT & PONDS	0.0070	0.21	15	1.93	0.07
POND AREA	0.4900	1.16	80	39.83	3.23
WAMSUTTER ROAD APPROACH	0.0050	0.10	7	2.47	0.07
DRILL SHOP CULVERT	0.0006	0.10	10	0.15	0.00

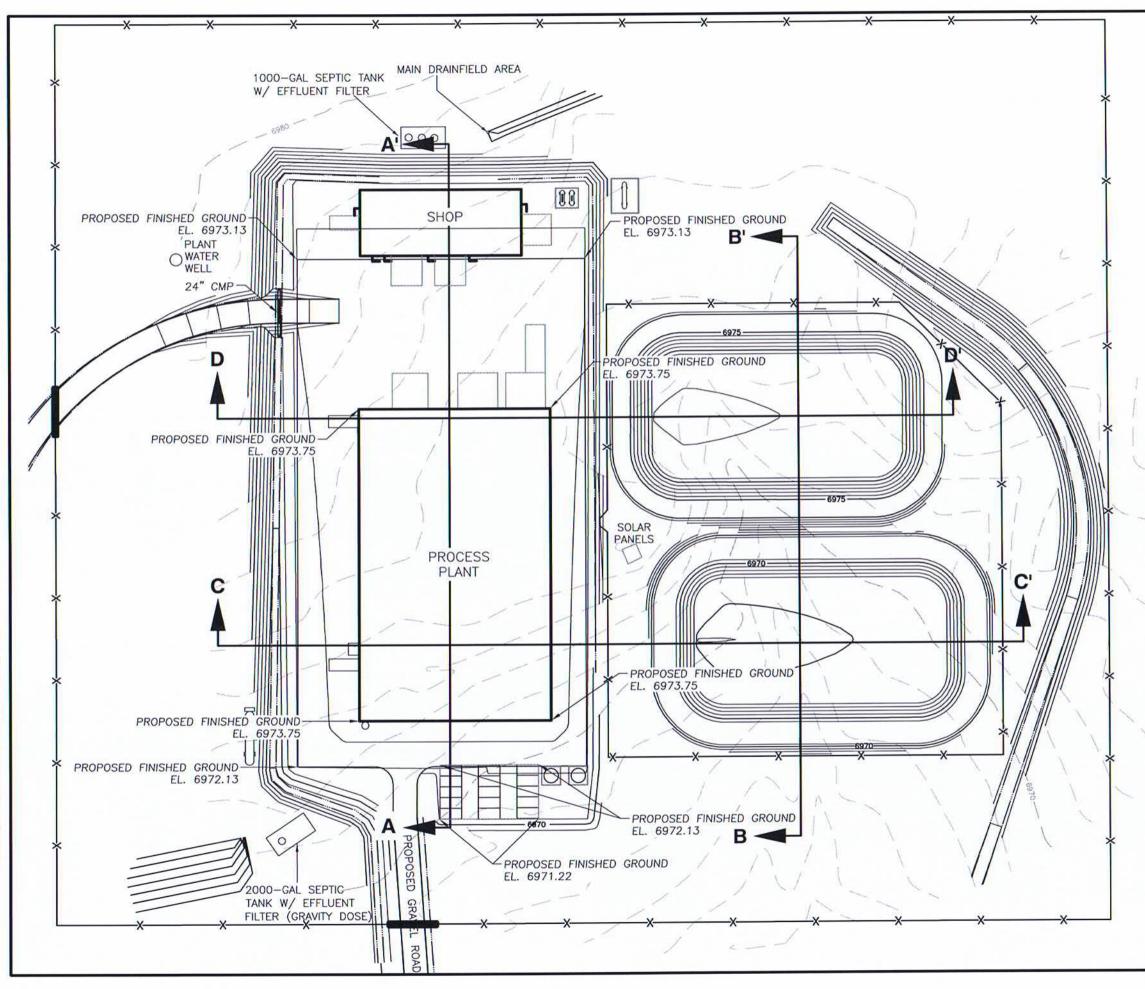
NOTE:

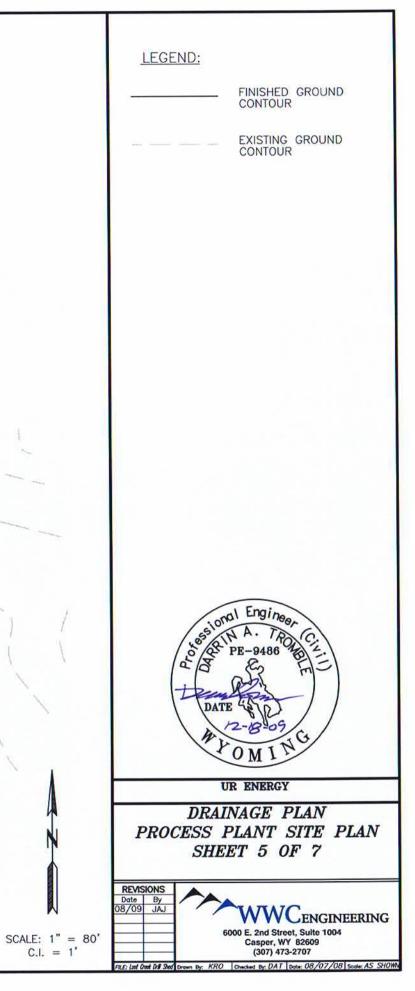
PEAK DISCHARGE AND RUNOFF VOLUME CALCULATED USING TRIHYDRO-98 FOR 25 YR 24 HR EVENT PIPE SIZES WERE CALCULATED USING PEAK DISCHARGES FROM TRIHYDRO IN FLOWMASTER

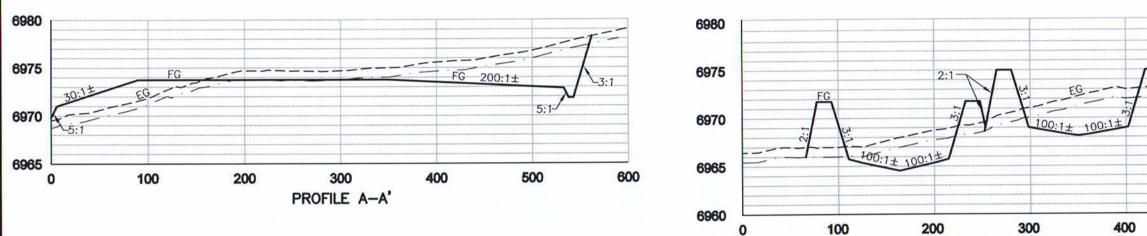




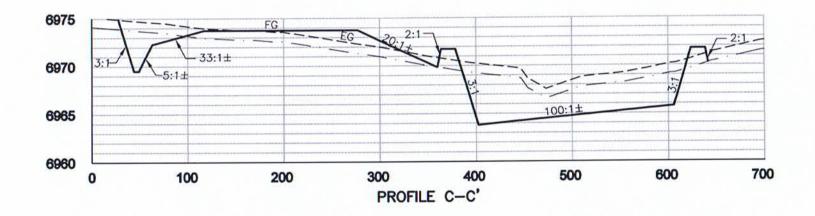


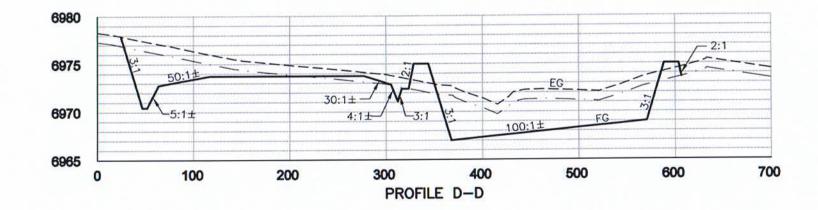


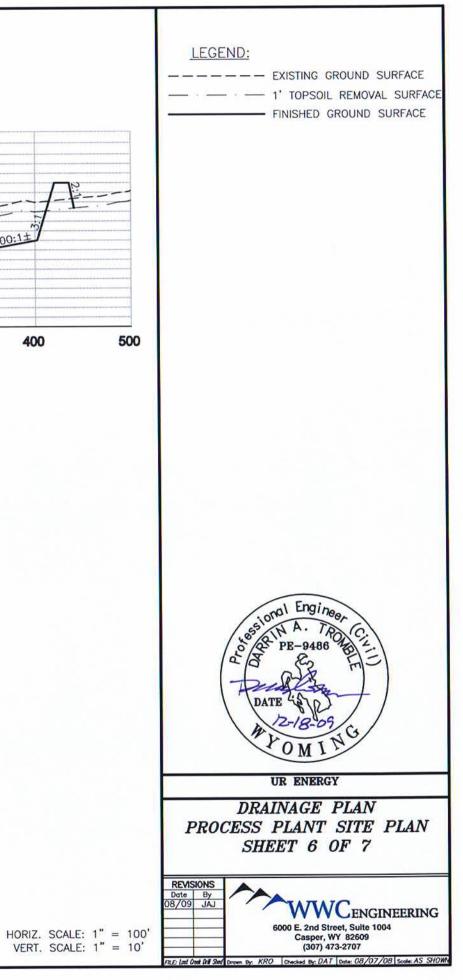


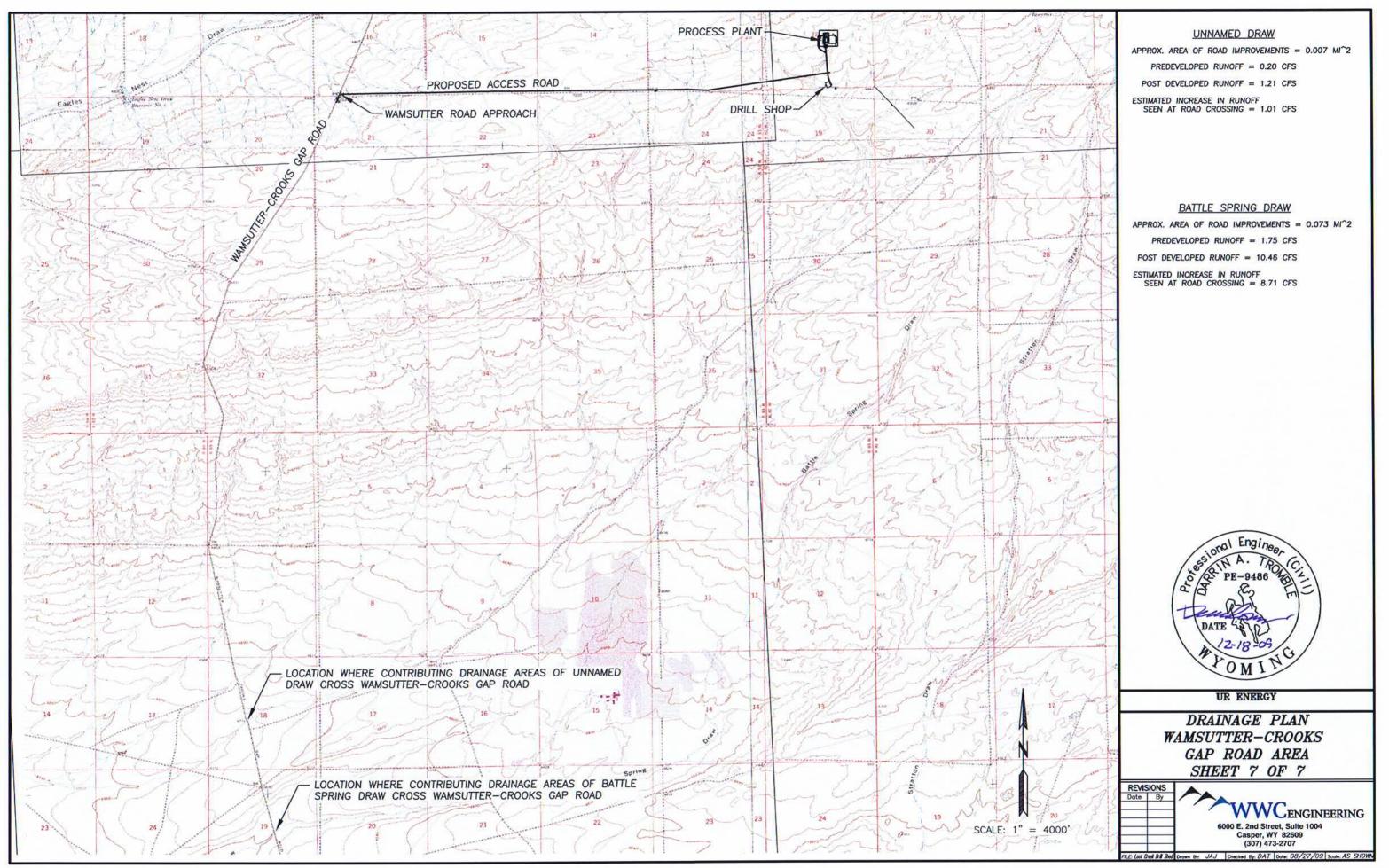


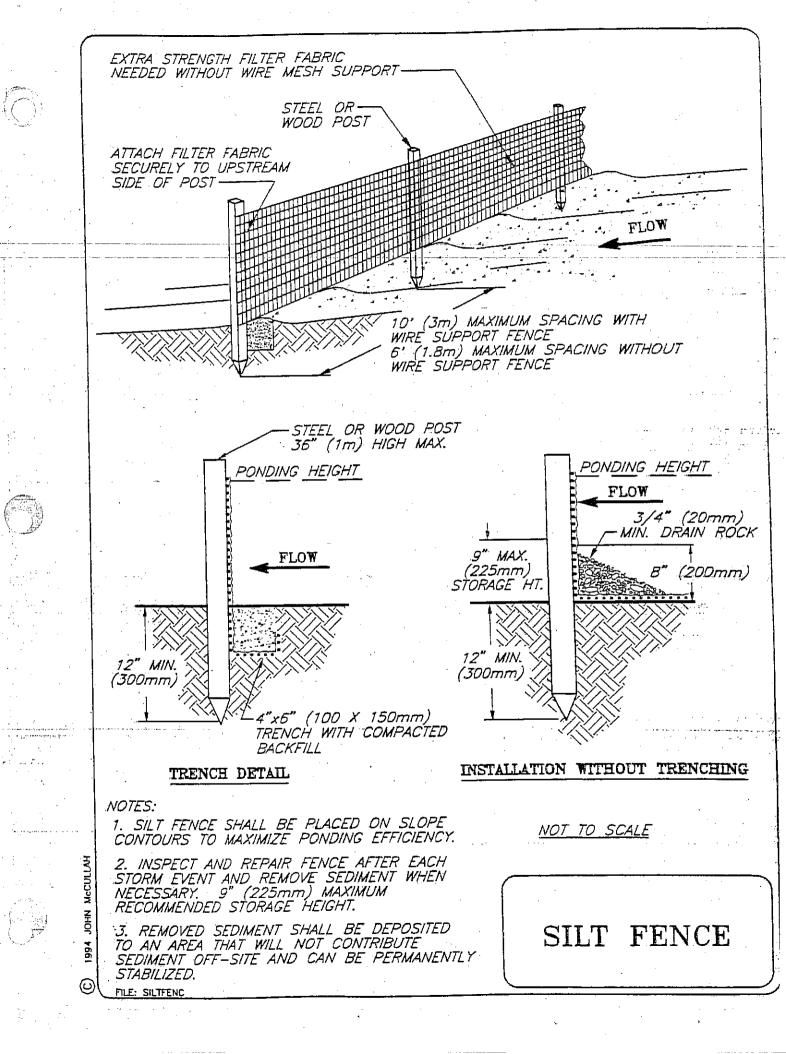
PROFILE B-B'

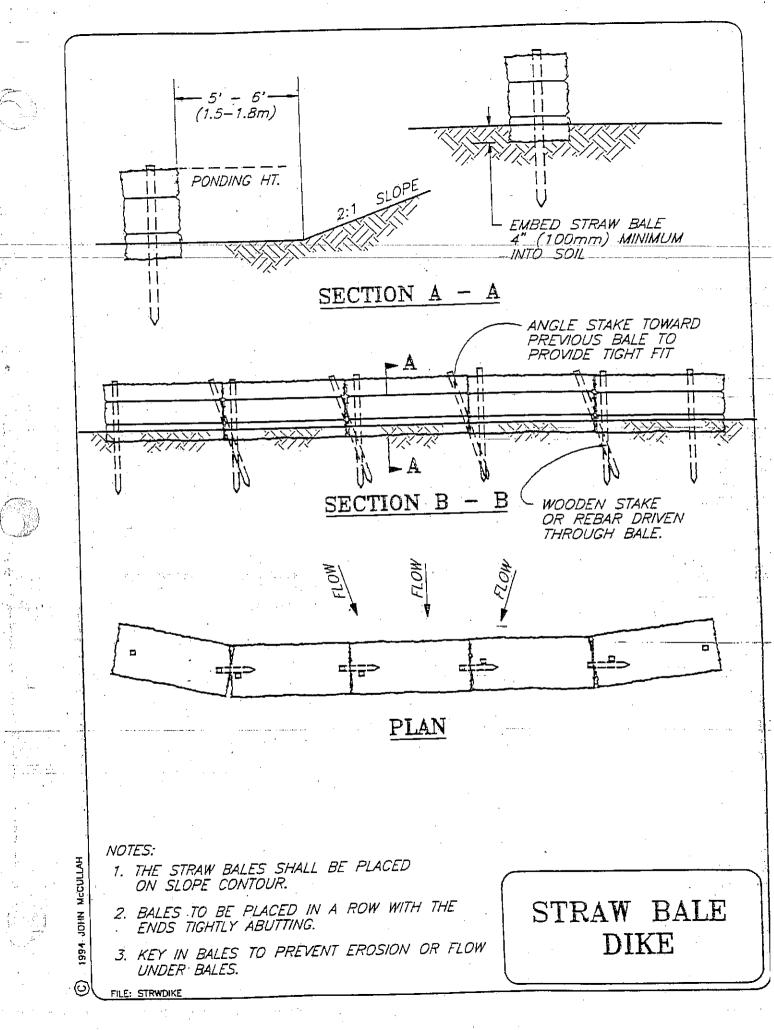












18" (0.5m)-+ 6" (150mm) 24" (0.6m) NOTE: KEY STONE INTO CHANNEL BANKS AND EXTEND IT BEYOND THE ABUTMENTS A MINIMUM OF 18" (0.5m) TO PREVENT FLOW AROUND DAM. VIEW LOOKING UPSTREAM FLOW 24" (0.6m) 8' (2.4m) · SECTION A - A 'L' = THE DISTANCE SUCH THAT POINTS 'A' AND B' ARE OF EQUAL ELEVATION. 41 ROINT 'B' POINT 'A' -SPACING BETWEEN CHECK DAMS McCULUAH a para di seri della ROCK NOT TO SCALE NHOP CHECK DAM 1994 \odot FILE: RCKCHKDM